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### Main Body Aerodynamics

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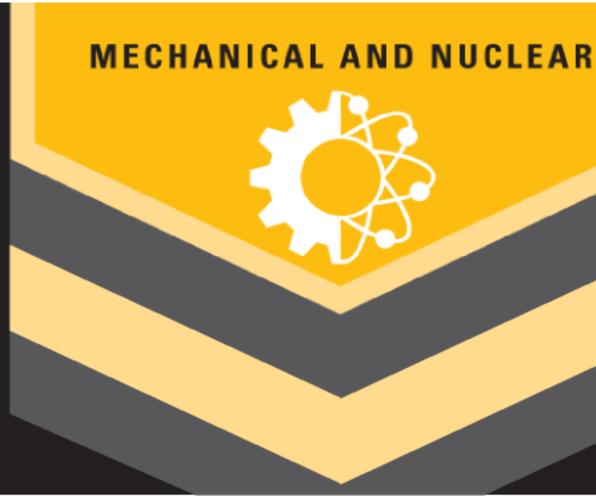
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# Introduction

Aerodynamic components are critical for the enhancement of the performance of and aesthetics of many vehicles. With the emergence of more accessible and intuitive computational fluid analysis software, Formula  $SAE_{\mathbb{R}}$  prototypes evolve aerodynamically each year.

# Objectives

- ➢ Induce downforce while reducing drag (obtaining a magnitude of lift to drag such that  $\frac{L}{D} \ge 2$  for the entire car)
- ➢ Generate an optimized spoiler profile for front and rear of vehicle
- ➢ Manage airflow around body of car through use of a front spoiler and diffuser combination
- $\succ$  Build prototypes and retrofit wind tunnel for comparative testing results and for the benefit of future VCU FSAE teams

# Conclusion

Overall, our design yielded a lift to drag ratio close to the desired value. We observed a strong correlation between the CFD and wind tunnel results for each component as well as collectively. However, the magnitude of lift to drag was proportionally lower in the wind tunnel experiment when compared to the computational results. This was due to factors only present in the physical experiment.







### **Mechanical Inputs**

Parameter	Input Value
Wheelbase	64in
Front Bulkhead L x W x H	28.00 x 15.20 x 15.30in
Rear Bulkhead L x W x H	15.80 x 13.50 x 10in
Total Frame Length	<b>95in</b>
Overall Frame Width	37in
Overall Frame Height	48in
Suspension Spring Rate	1.119 lbf/in

In order to meet both  $SAE_{\mathbb{R}}$  regulations and prototype chassis restrictions the design incorporated 3 key components:

**Velocity** R

**Spoiler W** 

Minimum

Temperatu

Pressure

Density

- Nose Cone and Side Panels
- Air redirection around chassis
- Drag reduction
- Rear Spoiler
- Induce downforce to driving wheels
- Mitigate effects of crosswinds/turbulence
- Front Spoiler
- air redirection for Lower body

Magnitude of Lift to Drag

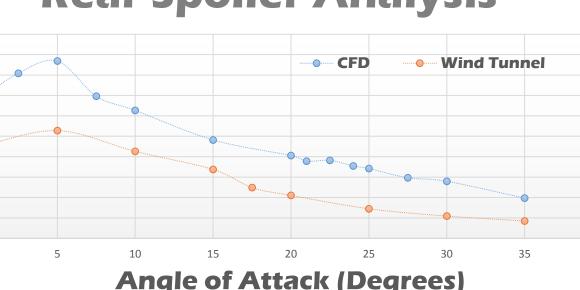
0.0482

3.079

2.463

1.863

- Balance forces induced by rear spoiler
- Swan-Neck Mounting Mechanism
- $\succ$  As a recent development in automotive aerodynamic design, the "swan neck" style of spoiler mount helps to reduce both drag and flow separation at the points of attachment to the spoiler planform, when compared to traditional mounting methods.



Main Body

Component

**Rear Spoiler (18°)** 

Front Spoiler (15°)

VIRGINIA

- Sources of Error
- wind tunnel testing due to vibrations scaled model
- > Achieving precise angle of attack on
- Geometric deformation to spoilers in
- Distribution of incoming flow on computational model
- Simplified recreation of boundary conditions (e.g. rolling floor)

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# School of Engineering

Overall

**Rear Spoiler Analysis** 



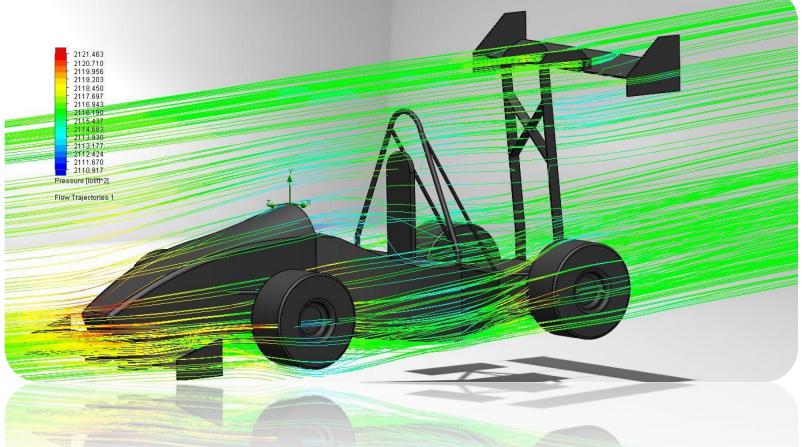
## **Fluid Dynamics Inputs**

rameter	Input Value
ange	20 < V < 80mph
dth	W ≤ 64in
Radii	R ≥ 0.060in
Properties of Air	
ure	68°F
	14.696 lbf/in <sup>2</sup>
	<b>3.612X10<sup>-5</sup> lb/in<sup>3</sup></b>



An optimized aerodynamic model was established utilizing a three pronged guide

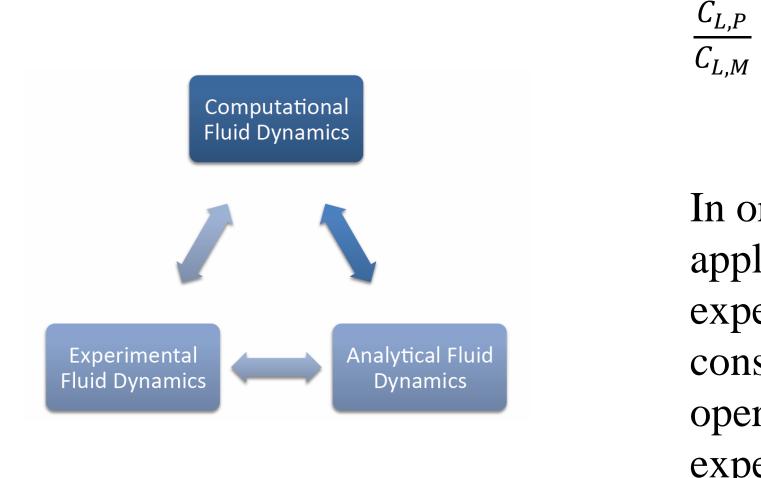
## Analytical Fluid Dynamics





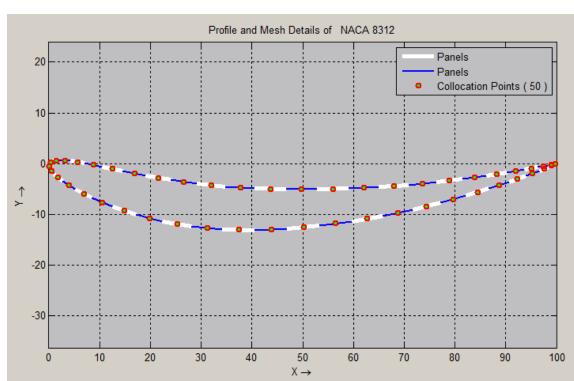
**Experimental Fluid Dynamics** 

> In order to provide an experimental comparison to our computationally generated designs, we performed a physical wind tunnel experiment. This utilized the Buckingham Pi Theorem by taking advantage of similarity conditions satisfied by the dimensionless coefficients of lift and drag.



## **Prototyping & Testing**

> Implemented more directly within the spoiler design process, the paneling method analytically determined a theoretically optimized, 2-D spoiler profile based on the desired lift to drag ratio. The nose cone and side panels were shaped initially by the physical restraints (attenuator and bulkhead) as well as the FSAE regulations.



### Computational Fluid Dynamics (CFD)

> With the ability to quickly alter geometries and obtain rapid analysis results, CFD allowed for numerous calculations of the lift forces and drag forces on the spoilers at different angles of attack and test their results prospectively.

$$\frac{1}{F} = 1 = \frac{\left(\frac{F_L}{\frac{1}{2}\rho v^2 A_s}\right)_p}{\left(\frac{F_L}{\frac{1}{2}\rho v^2 A_s}\right)_M}$$



In order to apply this theory, we implemented a scaling application of dimensionless analysis by performing our experiment at a 1/8 scale. Once a representative model was constructed, the wind tunnel was coupled with a sensor operating with a series of orthogonal strain rosettes to obtain experimental lift and drag forces.

Make it real.